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Spark plasma sintering of graphitized multi-walled carbon nanotube reinforced Ti6Al4V

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Abstract

Graphitized multi-walled carbon nanotubes (MWCNT_{Gr}) reinforced Ti6Al4V (Ti64) matrix composites prepared via the powder metallurgy route were synthesized by spark plasma sintering (SPS) technique. 1, 2 and 3 wt % MWCNT_{Gr} were dispersed in the Ti64 matrices by adapted high energy ball milling (HEBMA). Composite powder mixtures were sintered in vacuum at constant applied pressure, heating rate and isothermal holding time of 50 MPa, 100 °C/min and 5 min respectively. The sintering temperature was varied between 850 and 1000 °C. Scanning electron microscopy (SEM), transmission electron microscopy (TEM) and X-ray diffraction (XRD) were used to characterize the as-received MWCNTs, MWCNT_{Gr}, admixed composite powders and the bulk sintered composites. MWCNT_{Gr} evolution during graphitization treatment, dispersion in Ti64 matrix and in the sintered composites was analyzed using the characteristic Raman peak intensity ratio (I_D/I_G). The relative density of the sintered MWCNT_{Gr}/Ti64 composites was enhanced with increased sintering temperature, but deteriorated with increased wt % MWCNT_{Gr} in the metal matrix. Vickers microhardness of the consolidated composites improved with increasing sintering temperature and weight fractions of MWCNT_{Gr} over that of the unreinforced matrix alloy. The formation of crystalline TiC interfacial product during composite powder processing and consolidation is also discussed.

Keywords: Metal matrix composites; Reinforcement; MWCNT dispersion; Interfacial reaction; Graphitization

1. Introduction

Aluminium (Al) and magnesium (Mg) light metals have been extensively studied as structural materials for aerospace applications, although they lack the strength and rigidity attainable with iron and steel [1]. Over the years, Al and its alloys have been the mostly employed promising lightweight materials in this industry for improved fuel efficiency and control of CO₂ emissions. However, they are seldom used lately due to the harsh, fluctuating and high operating conditions that aerospace materials are subjected to in service [2]. Hence, this pressing demand for high strength and lightweight materials has inspired researchers to find alternative materials for Al and its alloys in aerospace applications [3].

Recently, titanium (Ti) and its alloys have been explored in the aerospace industry for weight savings (to replace steel and Al primarily), space limitation (as Al alloys replacement), high operating temperature (Al, steel and Ni-based alloys replacement), corrosion resistance (to replace low alloy steels and Al) and composite compatibility (replace Al alloys) [2, 4]. Nevertheless, Ti materials do exhibit inferior hardness, Young's modulus, heat and wear resistances when compared to steel and Ni-based alloys [4-6]. Consequently, Ti-matrix composites (TMC) with different reinforcement materials such as TiB whiskers [7-9], TiC particles [10-12], SiC fibers [13, 14] and particles [15], TiB₂ [16], SiO₂ [17] and carbon nanotubes [5, 18] have been reported.

Among these reinforcement materials, the development of high performance, smart TMCs for diverse engineering applications have been modified with carbon nanotubes (CNTs) as reinforcement in recent years. CNTs are attractive from the point of view of their superior mechanical, thermal and electrical properties, high aspect ratios and low densities [19-23]. However, there are very few reports in literature on Ti metal matrix being reinforced with CNTs, due to the associated processing challenges often encountered when reinforcing metal matrices with CNTs [24].

The processing challenges reported in previous studies are (i) achieving and maintaining the homogeneous dispersion of CNTs in the metal matrix, (ii) damage to CNTs during processing resulting in interfacial reactions with the matrix and (iii) weak bonding with the matrix [19, 25, 26]. Also, Feng *et al.* [27] and Munir *et al.* [23] have reported that high sintering temperatures promote interfacial reaction between Ti and defective multi-walled CNTs (MWCNTs). To overcome these challenges, the use of graphitized MWCNTs (MWCNT_{Gr}) has been reported to be beneficial for controlling interfacial reactions with the metal matrix, while Ti and its alloys in combination with

the advantages derivable from powder metallurgy techniques can offer interesting possibilities to the development and fabrication of CNTs reinforced TMCs [5, 27].

Although a few reports are available in literature on the reinforcement of Ti matrix with MWCNTs, none of these studies has to date reported on the reinforcement of Ti64 with MWCNTs, to the best of our knowledge. In addition, Weston *et al.* [28] stated that little attention has been given to the processing of Ti alloy powders by the SPS route. Zhang *et al.* [29] also reported that a significant gap still exists in the fundamental understanding of the SPS mechanisms. This gap was attributed to the complex nature of the electrical, thermal and mechanical processes involved during SPS and their dependence on the SPS parameters. Consequently, the availability of data on SPS mechanisms during sintering processes are largely limited [29, 30]. Therefore, this present study explored the advantages of SPS (rapid heating rate, low sintering temperature, short sintering cycle and fast cooling rate) as an advanced sintering technique to synthesize admixed MWCNT_{Gr}/Ti64 metal matrix composite powders aimed at controlling the characteristic challenge of interfacial reactions in fabricating CNT reinforced TMCs. The influence of sintering temperature and weight fraction of MWCNT_{Gr} on the densification, microstructure, microhardness and fracture characteristics of the consolidated composites were investigated.

2. Experimental

The starting powder materials used for this study were MWCNTs (Cheap Tubes Inc., USA, with outside diameter (OD) = 20–30 nm, length (L) = 10–30 μ m, ash < 1.5 wt %, purity > 95 wt %) and argon atomized, prealloyed Ti64 (-25 μ m particle size), supplied by TLS Technik GmbH & Co., Germany. The as-received MWCNTs were graphitized by high-temperature annealing for 5 h at 1800 °C in vacuum, using a Webb 77 Natick MA, USA tube furnace. The heating rate to the graphitization temperature was set at 10 °C/min.

Thereafter, the Retsch PM 400 MA, Germany, high energy ball mill (HEBM), was adapted for the mixing and dispersion of 1, 2 and 3 wt % MWCNT_{Gr} in the Ti64 metal matrix. The dispersion parameters were chosen such that the ball mill was used as a mixing medium rather than as a milling medium. Thus, neither size reduction nor fracturing of the matrix powder particles was expected to occur. This was also done to minimize the generation of non-sp² structural defects in MWCNT_{Gr} and control interfacial reaction with the metal matrix during dispersion processing. Both the matrix alloy powder and the measured wt % MWCNT_{Gr} were charged into stainless steel vials (250 ml capacity) with stainless steel balls of three different sizes (diameter (d) = 3, 5 and 7 mm).

The reason for using three different ball sizes was to prevent the charged powders from cold welding and to increase the collision energy available to the powder particles[31, 32]. These were mixed for 6 h at a rotational speed of 50 rpm. The ball to powder ratio (BPR) used was 10:1 while the ball mill was set to stop at intervals of 10 min for every 10 min of mixing. This was done to avoid cold welding of the powders and also prevent them from getting heated up due to excessive frictional and impact forces from ball-powder-ball interactions.

The starting powders and the admixed MWCNT_{Gr}/Ti64 composite powders were characterized by scanning electron microscopes (High Resolution Field Emission SEM (JSM-7600F, JEOL, Japan) and Zeiss Ultra Plus, Germany)) with incorporated energy dispersive X-ray spectrometry (EDX) facilities. A transmission electron microscope (JEOL JEM-2100F) was employed to study the surface morphologies and microstructure of the powders. Structural changes and crystalline phase identification studies of the composite powders were also performed by X-ray diffraction (PANalytical Empyrean model), with Cu K α radiation ($\lambda = 0.154$ nm) at a scan rate of 1°/min over a 10-90° angular range. The results were analyzed with Highscore plus software. The MWCNT_{Gr} admixed composite powders were characterized by Raman spectroscopy (T6400 Jobin Yvon, HORIBA, Japan) with a 514.5 nm laser employing a 20x objective lens. The spectra range used, was between 200 and 2000 cm⁻¹.

The admixed MWCNT_{Gr}/Ti64 composite powders in this work were consolidated by a SPS model HHPD-25, FCT Germany. Predetermined amounts of the composite powders were poured into a Ø 40 mm graphite die targeted at 5 mm thickness after sintering. The quantity of powder Q , expected to attain a desired composite disc thickness T of the sintered sample when fully dense, was calculated from Eq. 1. D_c is the theoretical density of the composite and r is the radius of the graphite die. D_c is calculated from Eq. 2 according to the rule of mixtures. W_m and W_f are the weight fractions of the Ti6Al4V matrix and MWCNTs reinforcement powders used respectively. D_m and D_f are the densities of Ti6Al4V (4.43 g/cm³) and MWCNTs (2.1 g/cm³) respectively.

$$Q = D_c T \pi r^2 \quad (1)$$

$$\frac{1}{D_c} = \frac{W_m}{D_m} + \frac{W_f}{D_f} \quad (2)$$

Graphite foils were placed between the powder and the graphite die to prevent powder welding and ensure uniform current flow within it. Composite powders were sintered in successive runs

at constant heating rate, applied pressure and holding time of 100°C/min, 50 MPa and 5 min respectively in vacuum. The sintering temperature was varied between 850 and 1000 °C. An optical pyrometer embedded within the upper punch was used to record the temperature within the sample core as the sintering experiment progressed. A pre-compaction force of 10 kN was applied at the onset of the SPS cycle to create good electrical contact between the powder and the die assembly. The densities of the consolidated composite samples were measured following Archimedes' principle at room temperature according to ASTM B962. The recorded density was an arithmetic mean of five different measurements taken from the same sample. Relative densities were calculated as a percentage of the calculated composite theoretical densities.

Microhardness measurements were carried out on sectioned as-polished sintered sample surfaces at room temperature under a load of 500 gf and dwell time of 15 s, according to ASTM E384. The reported hardness value for each sample is an arithmetic mean of ten successive indentations made on the as polished sample surface. The microstructure, fracture surfaces, structural and crystalline phase changes and the evolution of MWCNT_{Gr} in the consolidated samples were characterized by SEM, XRD and Raman spectroscopy respectively. The mirror polished samples were etched with Kroll's reagent (6 ml HF, 12 ml HNO₃ in 150 ml H₂O) before SEM analyses were carried out on them.

3. Results and discussion

3.1. Characterization of starting and admixed composite powders

Fig. 1 shows the morphologies of the starting powders used in this study. The as-received Ti64 metal matrix alloy powder (Fig. 1a) has spherical shaped particles (particle size = -25 µm and particle size distribution (PSD): D10 = 9.12 µm, D50 = 19.04 µm and D90 = 28.01 µm) characteristic of a gas atomized process. There was no evidence of agglomeration in the particles. The SEM image of the as-received MWCNT is presented in Fig. 1b, while its TEM image is shown in Fig. 1c. The MWCNTs are highly entangled and contained some amorphous carbon, retained metal catalysts and carbonaceous nanoparticles (these are seen as black spots, indicated by arrows in the TEM image) as identified from previous studies [28, 33].

The SEM micrograph of MWCNT_{Gr} is shown in Fig. 2a. The Raman spectra of the as-received MWCNTs and the MWCNT_{Gr} are presented in Fig. 2b. As previously suggested by [27], the quality

of MWCNTs is improved when subjected to graphitization treatment. This helps to reduce defects in MWCNTs and control interfacial reactions with metal matrices during processing.

The MWCNT_{Gr} (Fig. 2b (ii)) had two characteristic graphitic peaks at 1340 and 1570 cm⁻¹, which corresponds to the D and G bands respectively [34, 35]. The MWCNT_{Gr} showed a higher intensity G band peak at a wavenumber of 1570 cm⁻¹ compared to that exhibited by the as-received MWCNTs at 1565 cm⁻¹ (Fig. 2b (i)). Although the observed shift to a higher wavenumber in MWCNT_{Gr} has been attributed to stresses induced during treatment [36], the increase in the G band peak height is rather an indication of higher graphite crystallization and chemical stability [27]. The Raman peak ratio (I_D/I_G) reduced from 0.9 in the as-received MWCNTs to 0.8 in the MWCNT_{Gr} translating to 11 % improvement in graphite crystallization and increased graphite formation. This is evident in the narrower G band peak for the MWCNT_{Gr}.

Fig. 3 shows the SEM micrographs of the admixed MWCNT_{Gr}/Ti64 composite powder taken at low and high magnifications after 6 h mixing in the planetary ball mill. The dispersed MWCNT_{Gr} powders were seen coating the Ti64 particles (indicated by arrows in Figs. 3a-c). The higher magnification images (Figs. 3d-f) showed unbundled MWCNT_{Gr} (indicated by arrows) were dispersed in the Ti64 matrices at the different wt % MWCNT_{Gr} in the matrix alloy. However, it was observed that the degree of MWCNT_{Gr} dispersion reduced with the increased wt % MWCNT_{Gr} in the metal matrix. The MWCNT_{Gr} were relatively dispersed homogeneously in the composite powder with 1 wt % MWCNT_{Gr} (Fig. 3d) while clustered and agglomerated MWCNT_{Gr} (indicated by “P”) were observed in the composite powders with 2 and 3 wt % MWCNT_{Gr} respectively (Figs. 3e-f). This difficulty in unbundling MWCNT_{Gr} as its wt % increased within the matrix was partly due to the high aspect ratio, large surface area and the nano-size dimensions of MWCNT_{Gr}. Other factors include the characteristic tubular morphology and predominantly strong Van der Waals forces in the individual tubes which become stronger with the increased amount of MWCNT_{Gr} in the matrix [24, 37, 38].

Despite the fact that the MWCNT_{Gr} were dispersed into the matrix powder by dry HEBM_A and without the use of any PCA, there was no trace of cold welding in the admixed composite powders and particles of the metal matrix alloy maintained their original sizes and structure reasonably (Figs. 3a-c). No fracturing of the particles occurred. The presumed mechanism of MWCNT_{Gr} dispersion in Ti64 matrix was by diffusion (a gentle random motion distributing individual Ti64 particles throughout the powder mixture), convection (fast random motion which breaks down and

distributes agglomerates of CNT into the powder mixture) and shear (enhanced or robust particle movement by agitation, caused by powder-to-powder, powder-to-ball and powder-ball-vial wall interactions) as opposed to plastic deformation, welding and fracturing. It was affirmed that the dispersion process parameters used in this study during HEBM_A actually promoted the dispersion of MWCNT_{Gr} by mixing rather than milling. This observation is a significant departure from most of the available previous studies where mild to severe cold welding was reported during either dry or wet dispersion of MWCNTs in Ti matrices by HEBM, even in the presence of a PCA [31, 37-39]. However, the result of this present study agrees with the previous study by Bhat *et al.* [19] in which CNTs were dispersed into Cu–10Sn using a twin-roller mixer. It was reported that physical blending/mixing in the twin-roller mixer resulted in uniform and attachment of CNTs to the Cu–10Sn alloy powder without significant change in shape or size of the alloy powder.

The X-ray diffraction patterns of MWCNT_{Gr}, as-received Ti64 and the admixed MWCNT_{Gr}/Ti64 composite powders are shown in Fig. 4. The composite powders showed α -Ti peaks only, without evidence of peak broadening. This further corroborates the earlier position that there was no significant reduction in the sizes of the matrix Ti64 powder particles. MWCNT_{Gr} peaks were not seen in the XRD patterns of the admixed composite powders. This may be due to the XRD limit of detection which is not sufficient to detect small fractions of the MWCNT_{Gr} in Ti64 matrix powders. It could also be as a result of the wide difference in the mass absorption coefficients of Ti and carbon (for Cu K α radiations) that are 208 and 4.6 m²g⁻¹ respectively, which often makes it difficult for XRD to detect C in the presence of Ti [23, 40, 41]. Furthermore, it may be inferred from similar work by Cai *et al.* [20], that the absence of MWCNT peaks in the XRD patterns could also be due to the homogeneous dispersion of MWCNT_{Gr} in the Ti64 matrix or the amorphization of the MWCNT_{Gr}. Amorphization of CNTs describes the process of making the structure of CNTs become amorphous, that is, any process that generates the presence of non-sp² disorders/defects in the C-C network structure of CNTs. Ferrari and Robertson [42] identified three series of defects introduction in carbon based materials. These are: (i) bond-angle disorder, (ii) bond-length disorder and (iii) hybridization. A three-stage model for a typical amorphization trajectory was proposed by Lespade *et al.* [43] as: graphite \rightarrow nanocrystalline graphite (nc-G), nc-G \rightarrow a-C (amorphous carbon), and a-C \rightarrow ta-C (tetrahedral amorphous carbon; where there is $\sim 85\%$ sp³ ta-C). An example of amorphization occurs during dispersion processing of CNTs into metal matrices. Munir *et al.* [44] have demonstrated this in their previous study. They stated that structural

defects in MWCNTs may emerge mainly because of the energy absorbed by them during milling process via milling balls and the friction among MWCNTs and neighboring Ti particles resulting to the formation of highly reactive sp^3 C-C amorphous phases in MWCNTs.

Fig. 5 shows the results of the TEM observations conducted on the composite powders. For the powder containing 1 wt % MWCNT_{Gr} in the Ti64 alloy matrix, unbundled MWCNT_{Gr} were well dispersed in the metal matrix as seen in Figs. 5a–b. Deformed MWCNT_{Gr} was observed (indicated with arrow) in Fig. 5c. This kind of structural defect in the C–C network of MWCNT_{Gr} may be formed due to absorbed energy from the balls and frictional forces among neighboring Ti64 particles and MWCNT_{Gr}. This defect area is a potential site for the formation of interfacial products (such as TiC), owing to the interaction between the non- sp^2 carbon defects and the Ti64 particles [44]. However, as the wt % of MWCNT_{Gr} increased to 2 wt % in the matrix powder, a large agglomerate of MWCNT_{Gr} was observed in the matrix alloy (Fig. 5d). Fig. 5e also shows MWCNT_{Gr} in a large Ti64 particle. This suggests that the degree of dispersion of the MWCNT_{Gr} reinforcement powders in the metal matrix reduced with the increased wt % of the MWCNT_{Gr} in the matrix. Fig. 5f shows some deformed MWCNT_{Gr}. Nevertheless, individual nanotubes still maintained their tubular structure after the dispersion process. This is essential in order to ensure that the properties of interest in nanotubes are not lost. Otherwise, the properties and integrity of the final bulk composite will be compromised [23, 36, 38]. The severity of MWCNT_{Gr} destruction also increased with the increase in the weight fraction of the MWCNT_{Gr} reinforcement in the metal matrix (Figs. 5f and i). This was attributed to the increased difficulty in unbundling MWCNT_{Gr} due to stronger Van der Waals forces. There is a higher tendency for agglomeration of the MWCNT_{Gr}. Hence, the increased interaction between the metal particles and MWCNT_{Gr} on one hand and between individual hard MWCNT_{Gr} among themselves led to the observed defects in the MWCNT_{Gr}. However, no interfacial reaction products were observed in the TEM images which is in agreement with the XRD results earlier discussed in Fig. 4.

3.2. X-ray diffraction patterns of sintered Ti64 and MWCNT_{Gr}/Ti64 composites

The results of the analyses on the structural changes and crystalline phase evolution in the sintered unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites as characterized by XRD are shown in Fig. 6. Fig. 6a revealed that the sintered unreinforced Ti64 contained the characteristic α - and β -Ti phases of Ti64 with the matrix being the α -phase. There was no visible evidence of peak broadening in the peaks as the sintering temperature increased. The addition of MWCNT_{Gr} to Ti64 (Fig. 6b-d)

however showed the presence of crystalline TiC phases in the sintered composites aside from the α - and β -phases. It was observed that the TiC formation was dependent on sintering temperature and the weight fraction of MWCNT_{Gr} in the composites. No TiC was formed in the composites below 900 °C at all the weight fractions of MWCNT_{Gr} contained in the sintered composites. However, this does not suggest that TiC interfacial product could only be formed below 900 °C when defective MWCNTs react with Ti metal. Nevertheless, the observation in this present study agrees with the previous study by Feng *et al.* [27], in which they concluded the reaction between defective graphitized MWCNTs and Ti is promoted by an increase in temperature and that the amount of TiC formation is limited below 980 °C. Although an earlier report by Cai *et al.* [20] indicated that the reaction between Ti and amorphous carbons in defective MWCNTs can occur at a temperature as low as 700 °C during SPS processing, this present study showed that the HEBM_A method in combination with SPS can delay, and as well control, the interfacial reaction between Ti64 and defective MWCNT_{Gr}. This affirms the findings of a similar study by Wang *et al.* [45] wherein they opined that short sintering cycles in SPS preserve the structure of MWCNTs and may prevent the reaction between Ti and MWCNTs.

It was noticed that TiC only began to form in the composite with 1 wt % MWCNT_{Gr} at 950 °C, even though the crystalline phase was observed in the other composites containing higher MWCNT_{Gr} weight fractions at a lower temperature of 900 °C. This suggests that a higher amorphous carbon content in the MWCNT_{Gr} reinforcement caused by damages during powder processing (owing to difficulty in un-bundling and achieving adequate dispersion of MWCNT_{Gr}) at increased weight fractions of MWCNT_{Gr} lowers the activation energy needed for the TiC phase formation during sintering. Consequently, the reaction temperature between the defective MWCNT_{Gr} and Ti64 was lowered as it is presumed that the amount of defective MWCNT_{Gr} available for reaction with Ti64 particles is directly proportional to the weight fractions of MWCNT_{Gr} in the composites. This corroborates the position reported by Munir *et al.* [23, 38] that interfacial reactions during high temperature composite processing are triggered by the presence of severely deformed MWCNTs in a Ti matrix.

The XRD patterns of the composites containing 1 and 2 wt % MWCNT_{Gr} respectively showed peaks of retained MWCNT_{Gr} between 900 and 1000 °C. This high temperature retention of MWCNT_{Gr} as stated previously [20] is an indication that the interfacial reaction between MWCNTs and metal matrices can be controlled by improving the MWCNTs quality. This assertion is

supported by the results obtained from this present study as the TiC peaks in the sintered composites showed less intense peaks, suggesting that the interfacial reaction was largely controlled.

3.3. Microstructure of sintered Ti64 and MWCNT_{Gr}/Ti64 composites

The secondary electron images (SEI) of unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites (with varied weight fractions of the MWCNT_{Gr} reinforcements), sintered at 850 and 1000 °C respectively are shown in Fig. 7. The unreinforced Ti64 sintered at 850 and 1000 °C showed a near lamellar and fully lamellar microstructure respectively, with the characteristic Widmanstätten (basket weave) $\alpha+\beta$ network structure of Ti64 (Figs. 7a and b). The α -phase (grey) matrix contained the β -phase (white) on the α grain boundaries. At 1000 °C (Fig. 7b), the Widmanstätten-like microstructure is more prominent with the β -phase more elongated. There are more pores in the microstructure at 850 °C, whereas the pores are fewer and closed up at the higher sintering temperature. This is expected as sintering kinetics and atom diffusion are enhanced at high temperatures.

With the addition of MWCNT_{Gr} to Ti64, the micrographs of the sintered composites exhibited equiaxed microstructures consisting of α and β phases. They showed similar pore characteristics as the sintered unreinforced Ti64 at 850 and 1000 °C respectively. However, it was observed that at the lower sintering temperature, the amount of pores in the composites increased with the increasing weight fraction of MWCNT_{Gr}. This may be attributed to the difficulty in sintering due to insufficient diffusion between Ti64 and MWCNT_{Gr}, as well as the inadequate dispersion of MWCNT_{Gr} in the metal matrix owing to the re-agglomeration of MWCNT_{Gr} (depicted as retained CNT in Figs. 7e-g) as its weight fraction increased within the composites. This MWCNT_{Gr}-re-agglomeration is known to promote interfacial reaction with the metal matrix [37]. This can be ascribed to inadequate MWCNT_{Gr} dispersion during powder processing, which is evident from Figs. 3e and f. The effect of this is seen as the clustering of TiC particles in the composite with 3 wt % MWCNT_{Gr} (Fig. 7h) as the interfacial products are assumed to be formed around clustered retained MWCNT_{Gr}, which is in agreement with previous studies [37, 38]. The composite with 1 wt % MWCNT_{Gr} and sintered at 1000 °C showed a fully dense, fine, equiaxed $\alpha+\beta$ structure with no evidence of pores and retained (or re-agglomerated) MWCNT_{Gr}, which further affirms the effective dispersion of MWCNT_{Gr} during powder processing.

3.4. Raman spectra of sintered MWCNT_{Gr}/Ti64 composites

Raman spectroscopy has been a universally accepted tool for characterizing the evolution of the sp² C-C network of MWCNTs during composite processing [36, 37, 44]. In this study, it was necessary to first characterize the evolution of the MWCNT_{Gr} during the composite powder processing by HEBM_A, in order to fully understand the evolution of MWCNT_{Gr} in the sintered composites. Fig. 8 shows the Raman spectra of as-received Ti64, MWCNT_{Gr} and the admixed composite powders.

The Raman spectra of the as-received Ti64 powder (Fig. 8a) did not exhibit any peaks as Ti (similar to most metals) does not show active Raman vibrational modes [40]. Two graphitic peaks at 1340 and 1570 cm⁻¹ were seen in the MWCNT_{Gr} (Fig. 8b) as earlier stated. These correspond to the D and G bands respectively with I_D/I_G ratio = 0.8. The composite powder with 1 wt % MWCNT_{Gr} (Fig. 8c) had D and G bands respectively at 1342 and 1581 cm⁻¹. The shifting of the D band to a higher wavenumber was due to the stresses induced in the MWCNT_{Gr} during composite powder mixing [46, 47]. The characteristic I_D/I_G ratio increased to 1.01, which is a 26 % increase from that of the starting MWCNT_{Gr}. In a similar manner, I_D/I_G = 0.97 for the 2 wt % MWCNT_{Gr} composite powder. This translated to a 21 % increase compared to the as-received MWCNT_{Gr}, but is 5 % less than that for the composite powder with 1 wt % MWCNT_{Gr}. However, the I_D/I_G ratio for the composite powder with 3 wt % MWCNT_{Gr} could not be determined as the D and G band peaks had disappeared due to the amorphization of the MWCNT_{Gr}.

It is a generally accepted opinion that the structural integrity of MWCNTs is measured by the I_D/I_G ratio. The deterioration of MWCNTs in the form of non-sp² defects and other amorphous carbonaceous materials within MWCNTs make the intensities of the graphitic peaks in MWCNTs to diminish, that is, when I_D/I_G > 1. The more I_D/I_G < 1, the better is the structural integrity of the MWCNTs. Therefore, if the intensities of the graphitic peaks become so low that I_D/I_G cannot be determined, it then implies that the MWCNTs have become completely amorphous. Previous studies have indicated that significantly reduced Raman peaks in MWCNTs is an evidence of the extensive loss of crystallinity in MWCNTs and the presence of amorphous carbon phase [38, 42]. According to Ferrari and Robertson [42], the Raman spectrum is determined by four factors: (i) the clustering of the sp² phase, (ii) bond disorder, (iii) presence of sp² rings and chains, and (iv) the sp²/sp³ ratio. These factors act as controlling forces on the shape of the Raman spectra.

The D and G bands (Fig. 8) were progressively broadened with increasing wt % MWCNT_{Gr} in the metal matrix. Any broadening of the G band peak specifically is an evidence of induced disorders or loss of crystallinity as the G band represents the degree of pristine arrangement and crystallinity of the C-atoms in the graphitic network of MWCNTs[40]. It follows therefore, that the extensive loss of crystallinity and defect concentration due to amorphization of MWCNT_{Gr} increased with higher wt % MWCNT_{Gr} in Ti64 matrix during the mixing of the composite powders. Although the MWCNTs in the samples containing 1 and 2 wt % MWCNTs may have undergone amorphization also, the extent of amorphization is however directly proportional to the level of MWCNTs agglomeration. Furthermore, the higher the weight fraction of MWCNT in the matrix alloy, the more difficult it is to de-agglomerate or homogeneously disperse MWCNT in the Ti64 matrix. When CNTs are hugely agglomerated, interaction between the hard tubes due to high proximity leads to increased defects in the sp² C-C structure of the CNTs [23]. Therefore, it is expected that the sample with 3 wt % MWCNT will undergo the most amorphization.

Fig. 9 shows the Raman spectra of unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites sintered at 1000 °C. The sintered unreinforced Ti64 (Fig. 9a) as expected did not show any peaks since the alloy does not exhibit active Raman vibrational modes. The sintered composites containing 1 and 2 wt % MWCNT_{Gr} showed their D band peaks at the same wavenumber (1345 cm⁻¹) while their G band peaks were respectively at 1585 and 1574 cm⁻¹. Their I_D/I_G ratios also were 0.97 and 0.83 respectively. These values when compared with the I_D/I_G ratios for the corresponding composite powders after mixing as represented in Figs. 8c and d, showed that the I_D/I_G ratios reduced by 4 and 14 % respectively. The higher percentage reduction in the I_D/I_G ratio for the composite with 2 wt % MWCNT_{Gr} is justified as it exhibited a much higher G band peak intensity (Fig. 9c) which is an indication that the quality of MWCNT_{Gr} is preserved even at the highest sintering temperature of 1000 °C. The re-agglomerated or retained MWCNT_{Gr} had I_D/I_G = 0.83 after composite sintering, which is approximately the same as 0.8 for the as-received MWCNT_{Gr}.

The I_D/I_G ratio for the composite with 3 wt % MWCNT_{Gr} could not be determined, just as it was observed for the composite powders at this level after mixing. There were no visible D and G band graphitic peaks in this composite after sintering. It is an indication that the MWCNT_{Gr} were completely amorphous and extensively lost their crystallinity as a carryover of the damages to them during mixing. This suggests that non-sp² disorders in the C-C bond networks of MWCNT_{Gr} were prevalent in the composite powders after mixing. These disorders, as also reported

earlier[37], were responsible for initiating the interfacial reactions between the highly damaged MWCNT_{Gr} and Ti64 matrix particles during sintering at high temperature, leading to the formation of clustered TiC interfacial products as seen in Fig. 7h. The insufficient dispersion of MWCNT_{Gr} in the admixed composite powder (Fig. 3f) also enhanced this interfacial reaction [48]. The XRD scans (Fig. 6d) confirm these observations as there were no retained MWCNT_{Gr} peaks in the sintered composites.

3.5. Influence of sintering temperature on the densification of MWCNT_{Gr}/Ti64 composites

The densification patterns in the sintered composites and the unreinforced matrix alloy are shown in Fig. 10. The unreinforced Ti64 attained near theoretical density at all the sintering temperatures (850 – 1000 °C) investigated in this study. The relative density increased from 98.8 % to 99.6 % between 850 and 1000 °C translating to a 0.8 % increase. However, the measured relative density was constant between 900 and 950 °C, while only a 0.1 % increase (99.5 to 99.6 %) was observed between 950 and 1000 °C. Nevertheless, an increase of 0.7 % (98.8 to 99.5 %), which is almost equal to that observed between 850 and 1000 °C, was recorded between 850 and 900 °C. The enhancements in densification with increased sintering temperature were attributed to improved diffusion bonding and atom mobility at high temperatures. The closure of pores at high temperature as seen in the microstructures in Fig. 7b, is also responsible for the improved densification. This suggests that raising the sintering temperature was an effective route of densification enhancement for the matrix alloy.

The densification pattern in the sintered composites displayed a progressive reduction in the relative densities of the composites as the weight fractions of the reinforcement increased in the composites. This progressive reduction in the relative densities with increased MWCNT_{Gr} weight fraction may be attributed to the agglomeration and clustering of MWCNT_{Gr} in the metal matrix. It could also be due to weak interfacial bonding in the composites caused by the insufficient diffusion between Ti64 and MWCNT_{Gr}, which may result in thermal mismatch between the matrix and the reinforcement.

At 850 °C, sintered relative density decreased from 99.8 % in the unreinforced Ti64 to 96.3 % in the composite with 3 wt % MWCNT_{Gr}, translating to a 3.5 % reduction. At 1000 °C, the recorded reduction was 1.6 % (that is, from 99.6 to 98 %). The reduction in the measured relative densities as MWCNT_{Gr} weight fractions increased from 1 to 3 wt % at 850 and 1000 °C were 1.7 and 1.2 %, respectively. The relative homogeneous dispersion of MWCNT_{Gr} in the composite with 1 wt

% MWCNT_{Gr} (Fig. 3d) was responsible for its better relative density in comparison to the composites with 2 and 3 wt % MWCNT_{Gr} (Figs. 3e and f) respectively. These observations are in agreement with the reports of a similar study by Saheb *et al.* [49] on the reinforcement of Al alloys with CNTs. The higher relative density in the composite with 1 wt % MWCNT_{Gr} was most probably due to the relative homogeneous dispersion of the MWCNT_{Gr} within the metal matrix and not due to the supposed minor detrimental effect of a lower weight fraction of MWCNT_{Gr}. This position was premised on a previous study by Wang *et al.* [45] wherein the amount of MWCNT in pure Ti were 0.2, 0.4, 0.6, 0.8 and 1.0 wt %. The relative densities of the composites decreased with increasing wt % MWCNT (99.69, 99.44, 99.31, 99.13 and 99.01 %) respectively despite the small amounts of MWCNT used compared to those used in this present study. The report justifies the position intended in this current study that even very small increase of MWCNT in a metal matrix could be responsible for a decrease in relative density of the bulk composite. This is because the tendency for pre-agglomeration (during dispersion processing) and re-agglomeration of MWCNT (during SPS) increases with increased weight fractions of MWCNT in the metal matrix. All the composites in this study exhibited lower relative densities than the unreinforced alloy. However, they showed a similar trend of enhanced densification with increased sintering temperature. Between 850 and 1000 °C, the relative densities improved by 1.2, 0.5 and 1.7 % with 1, 2 and 3 wt % MWCNT_{Gr} respectively in the sintered composites.

3.6. Hardness of consolidated MWCNT_{Gr}/Ti64 composites

The variation of hardness in the sintered MWCNT_{Gr}/Ti64 composites and at different sintering temperatures, is presented in Fig. 11. It was observed that the hardness of the composites improved with increasing weight fractions of MWCNT_{Gr} added to the Ti64 matrix alloy at all the sintering temperatures investigated in this study. Between 850 and 1000 °C, the measured percentage increases in hardness were 2.2 (370 – 378 HV), 7.3 (369 – 396 HV) and 15.7 % (344 – 398 HV) as the weight fraction of MWCNT_{Gr} was increased from 1, 2 to 3 wt % respectively. Comparing the hardness of the unreinforced Ti64 and the composite containing 3 wt % MWCNT_{Gr} at 850 and 1000 °C respectively, the observed hardness was enhanced by 2.7 and 10 % respectively, as the measured hardness improved from 335 – 344 HV and from 362 – 398 HV at these temperatures respectively. The increase in microhardness with increased sintering temperature in both the unreinforced alloy and the composites was the result of pore closure and improved densification as the sintering temperature increased. The presence of the hard TiC interfacial

product with increasing sintering temperature (Fig. 6), also contributed to the increased hardness. However, the increase in hardness despite the loss in densification that was observed (Fig. 10) with the increased MWCNT_{Gr} weight fraction in the composites, was attributed to the presence of retained MWCNT_{Gr} and crystalline TiC hard phases which formed due to the interfacial reaction between the defective MWCNT_{Gr} and the metal matrix. These results are consistent with previous studies by [21, 50, 51].

3.7. Fracture characteristics MWCNT_{Gr}/Ti64 composites

The fracture surfaces of unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites sintered at 1000 °C are shown in Fig. 12. The fracture surface of the unreinforced Ti64 metal matrix alloy (Fig. 12a) showed typical dimpled fracture morphology of Ti and its alloys [50], suggesting that the sintered alloy underwent ductile fracture mode. Its particles were also well deformed (Fig. 12(a¹)) implying good sample cohesion as a result of better sinterability during the SPS processing. However, the sample containing 1 wt % MWCNT_{Gr} showed a more dimpled structure, which suggests improved sample cohesion and inherently good metallurgical bonding between the Ti64 matrix and MWCNT_{Gr} reinforcement. Fig. 12(b¹) showed the MWCNT_{Gr} still retained their sizes and structure, displayed good interfacial bonding with the matrix and were well-dispersed within the matrix. The binding strength displayed by this composite during fracture was attributed to these observed features. This is consistent with the findings of Wang *et al.* [45]. However, as the weight fraction of MWCNT_{Gr} increased to 2 and 3 wt % respectively in the Ti64 matrix, the dimples on the fracture surfaces of the composites reduced drastically (Fig. 12c-d), with only faint traces of the dimples left. This implies the fracture pattern in these samples were a combination of ductile and brittle fractures, the most prevalent being the latter. High magnification images of the areas within the white circles in Figs. 12c and d represented in Figs. 12c¹ and d¹ respectively showed highly agglomerated MWCNT_{Gr} that are isolated from the matrix. This is because it becomes increasingly difficult to effectively disperse MWCNT_{Gr} within the metal matrix as their weight fractions are increased in the composite matrix. This resulted in the observed weak interfacial bonding between the matrix and the reinforcement. Observing the fracture surfaces of these composites, the features displayed showed the prevalent fracture modes in these composites were MWCNT_{Gr} pull out from the matrix particles. That is, there occurs interfacial isolation of MWCNT_{Gr} from the Ti64 matrix, cleavage of Ti64 matrix particles and tensile fracture of MWCNT_{Gr}. These observations are in agreement with the conclusions previously reported by Wang *et al.* [45] and Li *et al.* [5].

4. Conclusions

Graphitized multi-walled carbon nanotube reinforced Ti64 composites were successfully synthesized by spark plasma sintering. The HEBMA method explored for the dispersion of MWCNT_{Gr} in Ti64 matrix ensured that no interfacial reaction between the metal matrix and defective MWCNT_{Gr} occurred during mixing. The presence of the retained MWCNT_{Gr} in the consolidated composites at high temperatures indicates that subjecting the MWCNTs to graphitization treatment in combination with composite consolidation by SPS can control or delay the interfacial reaction during sintering. The relative densities of the sintered composites improved with sintering temperature, but declined with increased weight fractions of MWCNT_{Gr} in the composites due to inadequate dispersion or re-agglomeration of the MWCNT_{Gr} and weak interfacial bonding between the matrix and reinforcement. The observed microhardness increased with increased sintering temperature and MWCNT_{Gr} weight fractions in the composites. The prevalent fracture mechanism in the composites was by MWCNT_{Gr} pull out from the matrix particles.

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FIGURE CAPTIONS

Fig. 1. SEM morphologies of starting powders: (a) Ti6Al4V, (b) highly entangled MWCNTs, and (c) TEM image of entangled MWCNTs.

Fig. 2. Morphology and evolution of MWCNT_{Gr} (a) SEM image of MWCNT_{Gr}, (b) Raman spectra of (i) as-received MWCNT and (ii) MWCNT_{Gr}.

Fig. 3. SEM micrographs of admixed MWCNT_{Gr}/Ti64 composite powders with varied wt % MWCNT_{Gr} in the metal matrix (a) 1 % wt MWCNT_{Gr}, (b) 2 % wt MWCNT_{Gr}, (c) 3 % wt MWCNT_{Gr}; (d) – (f) are the corresponding high magnification surface morphologies of the composite powders.

Fig. 4. XRD patterns of starting and admixed MWCNT_{Gr}/Ti64 composite powders (a) MWCNT_{Gr}, (b) as-received Ti64, (c) Ti64-1%MWCNT_{Gr}, (d) Ti64-2%MWCNT_{Gr} and (e) Ti64-3%MWCNT_{Gr}.

Fig. 5. TEM images of MWCNT_{Gr}/Ti64 composite powders with varied wt % MWCNT_{Gr}: (a) – (c) Ti64-1%MWCNT_{Gr}, (d) – (f) Ti64-2%MWCNT_{Gr}, (g) – (i) Ti64-3%MWCNT_{Gr}.

Fig. 6. XRD patterns of Ti64 and MWCNT_{Gr}/Ti64 sintered at different temperatures (a) Ti64, (b) Ti64-1%MWCNT_{Gr}, (c) Ti64-2%MWCNT_{Gr} and (d) Ti64-3%MWCNT_{Gr}.

Fig. 7. SEM images of Ti64 and MWCNT_{Gr}/Ti64 composites sintered at 850 and 1000 °C respectively: (a) as-received Ti64 at 850 °C, (b) as-received Ti64 at 1000 °C, (c) Ti64-1%MWCNT_{Gr} at 850 °C, (d) Ti64-1%MWCNT_{Gr} at 1000 °C, (e) Ti64-2%MWCNT_{Gr} at 850 °C, (f) Ti64-2%MWCNT_{Gr} 1000 °C, (g) Ti64-3%MWCNT_{Gr} at 850 °C and (h) Ti64-3%MWCNT_{Gr} at 1000 °C.

Fig. 8. Raman spectra of starting and MWCNT_{Gr}/Ti64 composite powders (a) as-received Ti64, (b) MWCNT_{Gr}, (c) Ti64-1%MWCNT_{Gr} (d) Ti64-2%MWCNT_{Gr}, (e) Ti64-3%MWCNT_{Gr}.

Fig. 9. Raman spectra of unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites sintered at 1000 °C (a) Ti64, (b) Ti64-1%MWCNT_{Gr} (c) Ti64-2%MWCNT_{Gr}, (d) Ti64-3%MWCNT_{Gr}.

Fig. 10. Densification patterns in unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites.

Fig. 11. Microhardness of MWCNT_{Gr}/Ti64 composites with varied weight fractions of MWCNT_{Gr} in Ti64 matrix.

Fig. 12. Fractured surfaces of (a) unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites with varied weight fractions of MWCNT_{Gr} (b) 1 wt % MWCNT_{Gr}, (c) 2 wt % MWCNT_{Gr}, (d) 3 wt % MWCNT_{Gr}, (a¹) – (d¹) are the corresponding SEM images of (a) – (d) taken at higher magnification respectively.

FIGURES

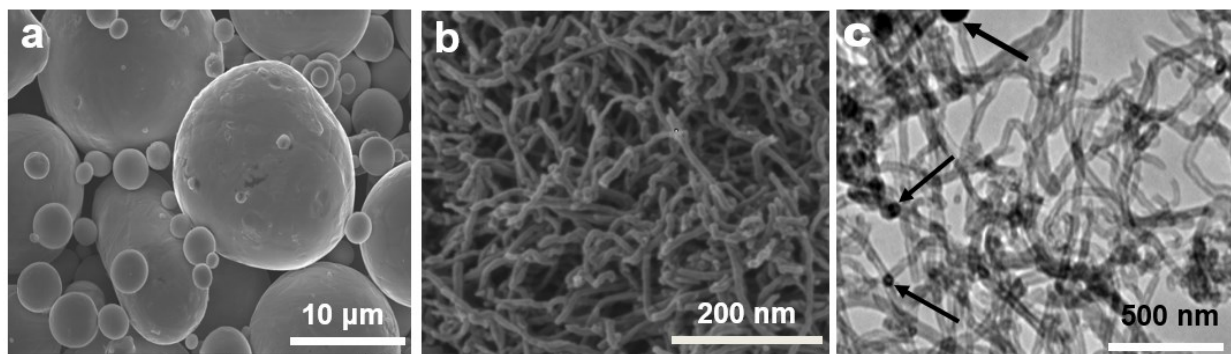


Fig. 1. SEM morphologies of starting powders: (a) Ti6Al4V, (b) highly entangled MWCNTs, and (c) TEM image of entangled MWCNTs.

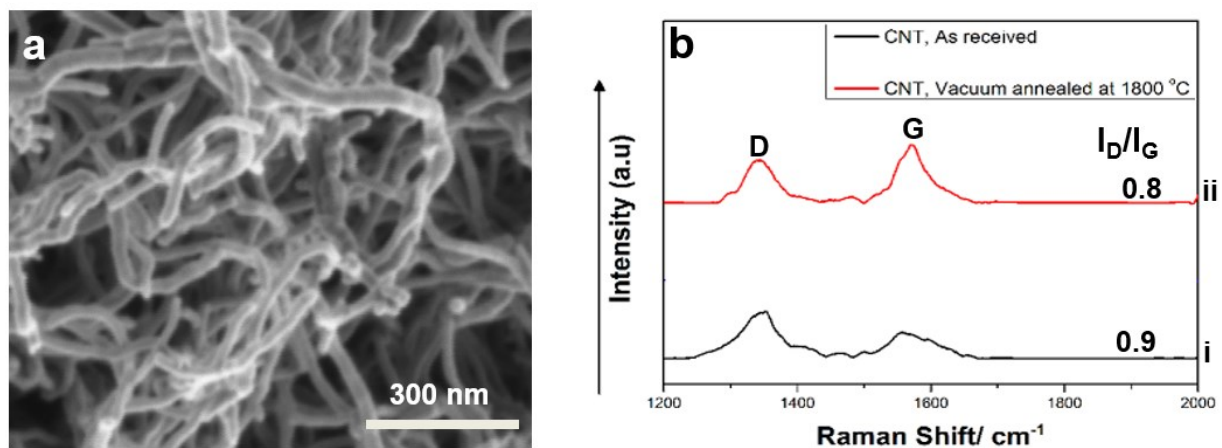


Fig. 2. Morphology and evolution of MWCNT_{Gr} (a) SEM image of MWCNT_{Gr} , (b) Raman spectra of (i) as-received MWCNT and (ii) MWCNT_{Gr} .

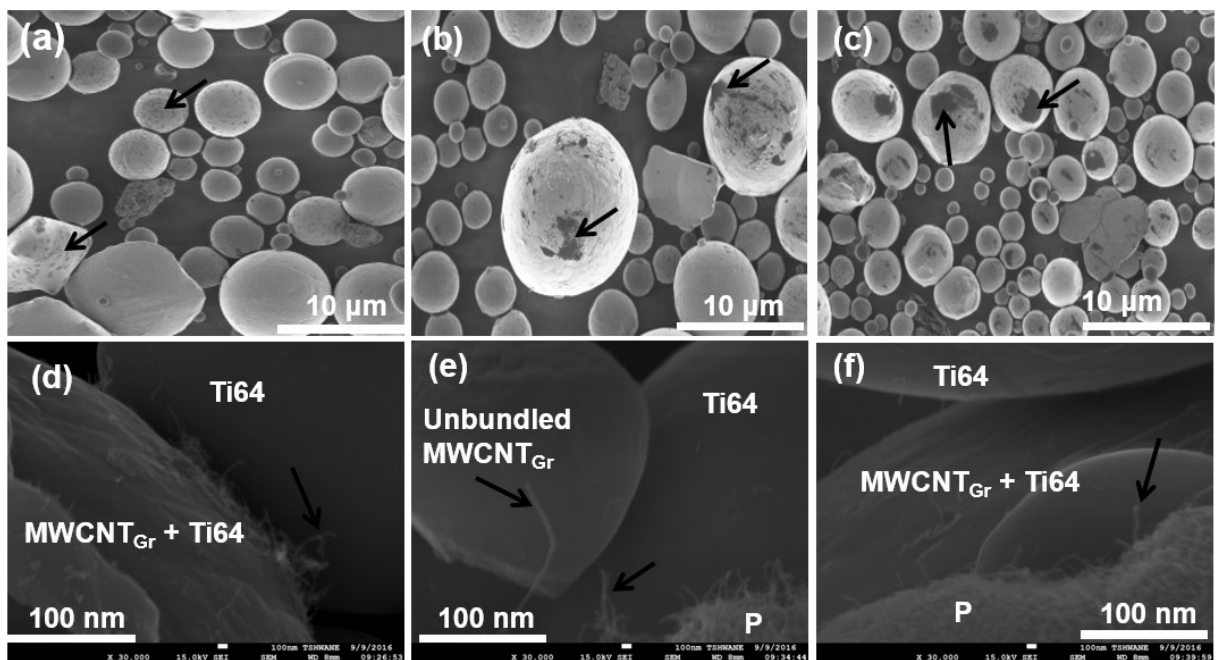


Fig. 3. SEM micrographs of admixed MWCNT_{Gr} /Ti64 composite powders with varied wt % MWCNT_{Gr} in the metal matrix (a) 1 % wt MWCNT_{Gr} , (b) 2 % wt MWCNT_{Gr} , (c) 3 % wt MWCNT_{Gr} ; (d) – (f) are the corresponding high magnification surface morphologies of the composite powders

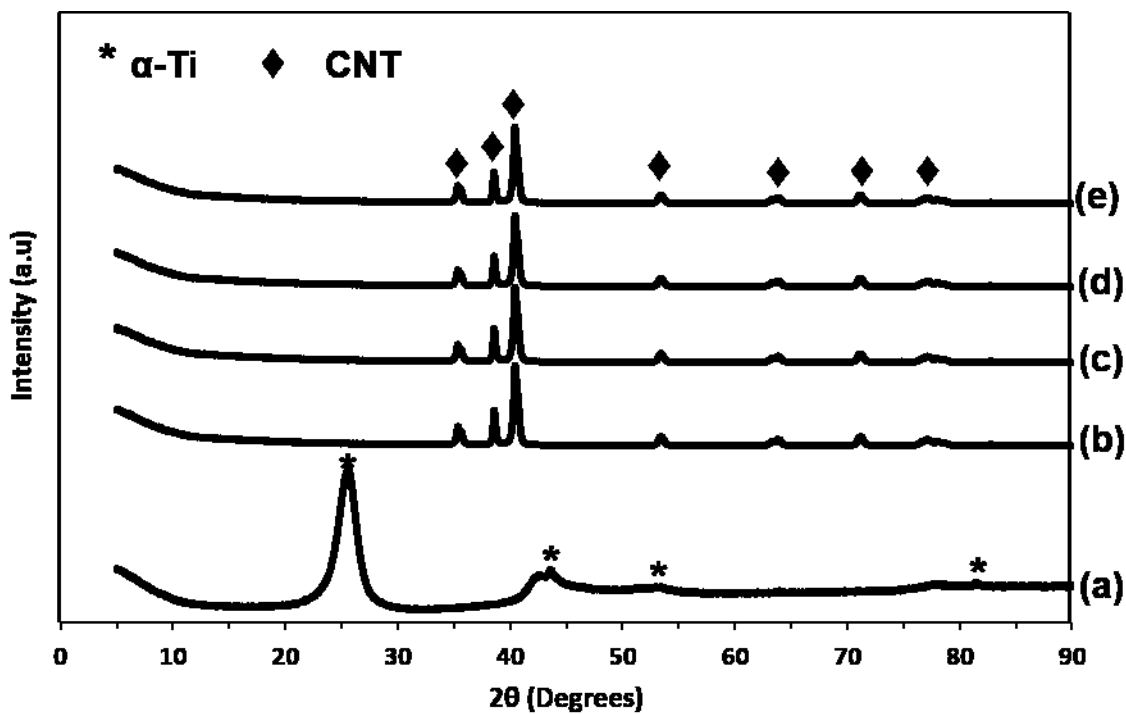


Fig. 4. XRD patterns of starting and admixed MWCNT_{Gr}/Ti64 composite powders (a) MWCNT_{Gr}, (b) as-received Ti64, (c) Ti64-1%MWCNT_{Gr}, (d) Ti64-2%MWCNT_{Gr} and (e) Ti64-3%MWCNT_{Gr}.

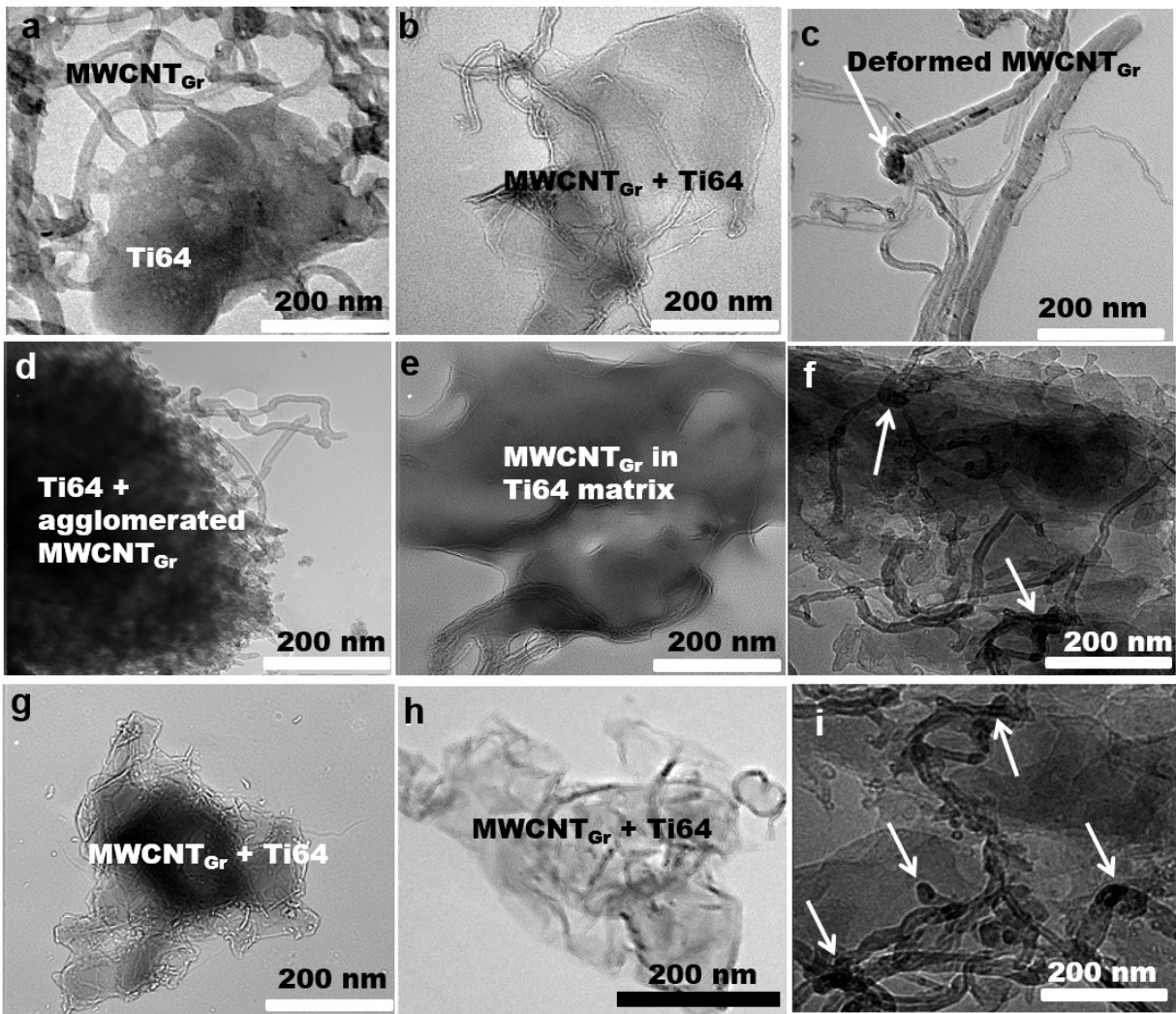


Fig. 5. TEM images of MWCNT_{Gr}/Ti64 composite powders with varied wt % MWCNT_{Gr}: (a) – (c) Ti64-1%MWCNT_{Gr}, (d) – (f) Ti64-2%MWCNT_{Gr}, (g) – (i) Ti64-3%MWCNT_{Gr}.

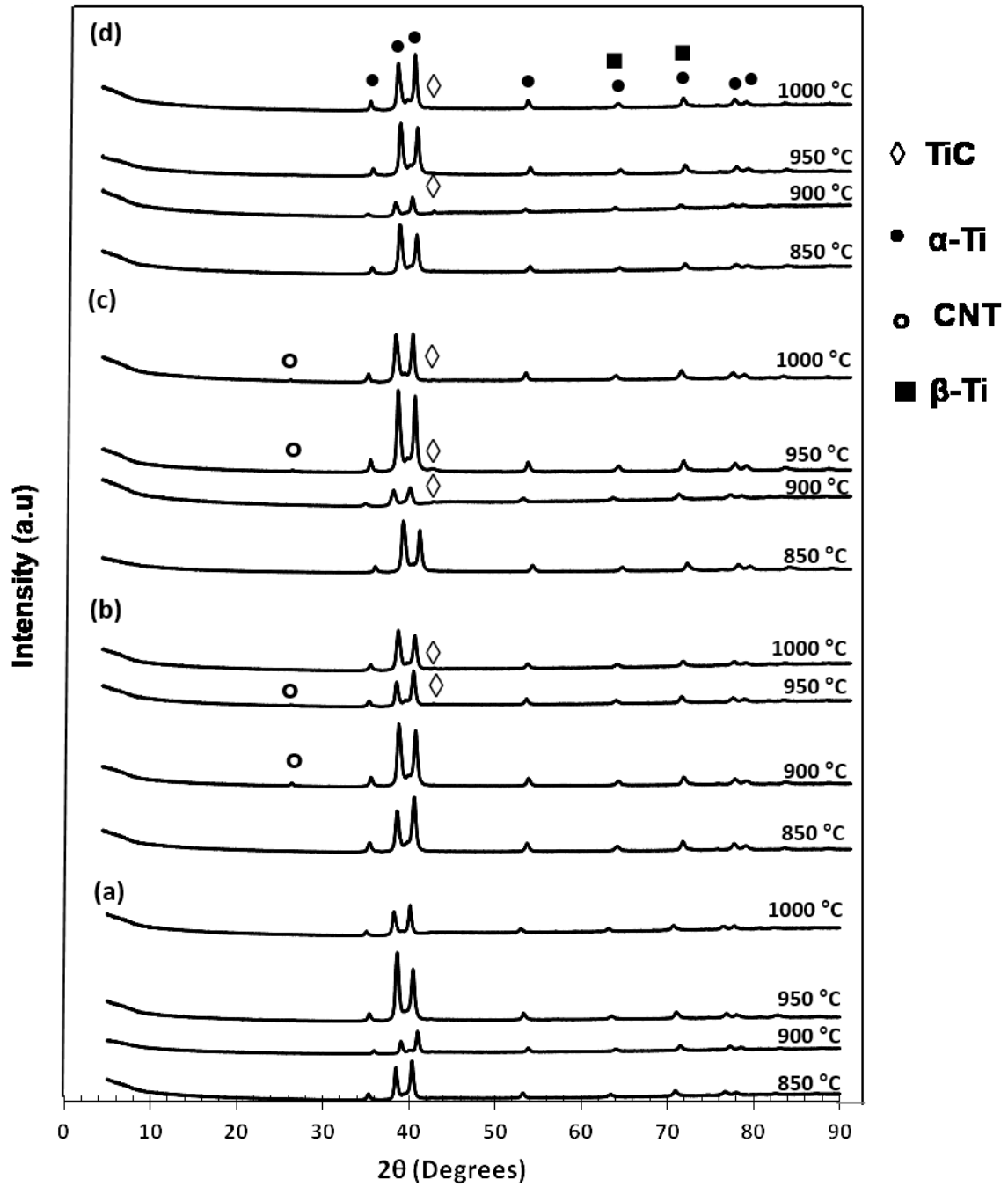


Fig. 6. XRD patterns of Ti64 and MWCNT_{Gr}/Ti64 sintered at different temperatures (a) Ti64, (b) Ti64-1%MWCNT_{Gr}, (c) Ti64-2%MWCNT_{Gr} and (d) Ti64-3%MWCNT_{Gr}.

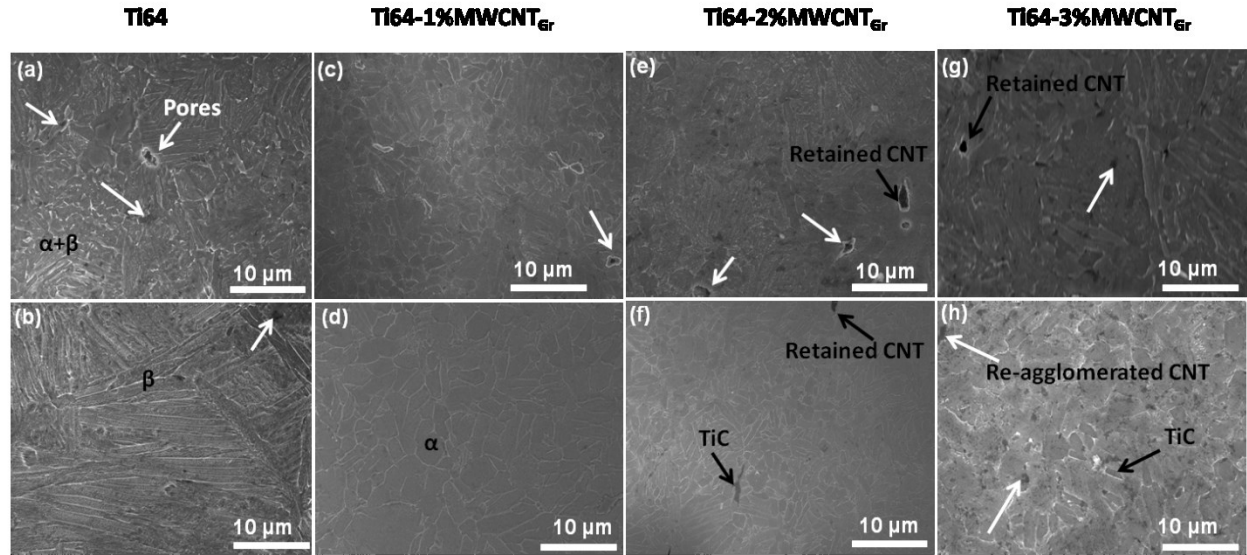


Fig. 7. SEM images of Ti64 and MWCNT_{Gr}/Ti64 composites sintered at 850 and 1000 °C respectively: (a) as-received Ti64 at 850 °C, (b) as-received Ti64 at 1000 °C, (c) Ti64-1%MWCNT_{Gr} at 850 °C, (d) Ti64-1%MWCNT_{Gr} at 1000 °C, (e) Ti64-2%MWCNT_{Gr} at 850 °C, (f) Ti64-2%MWCNT_{Gr} at 1000 °C, (g) Ti64-3%MWCNT_{Gr} at 850 °C and (h) Ti64-3%MWCNT_{Gr} at 1000 °C.

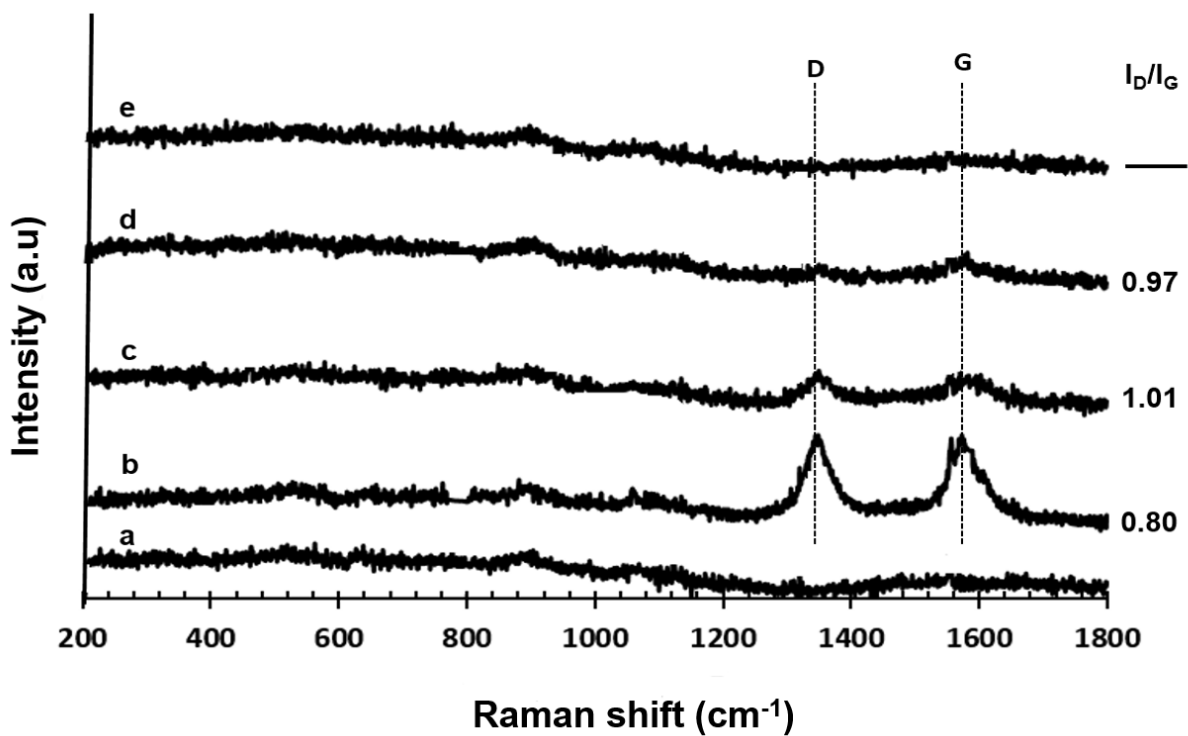


Fig. 8. Raman spectra of starting and MWCNT_{Gr}/Ti64 composite powders (a) as-received Ti64, (b) MWCNT_{Gr}, (c) Ti64-1%MWCNT_{Gr} (d) Ti64-2%MWCNT_{Gr}, (e) Ti64-3%MWCNT_{Gr}.

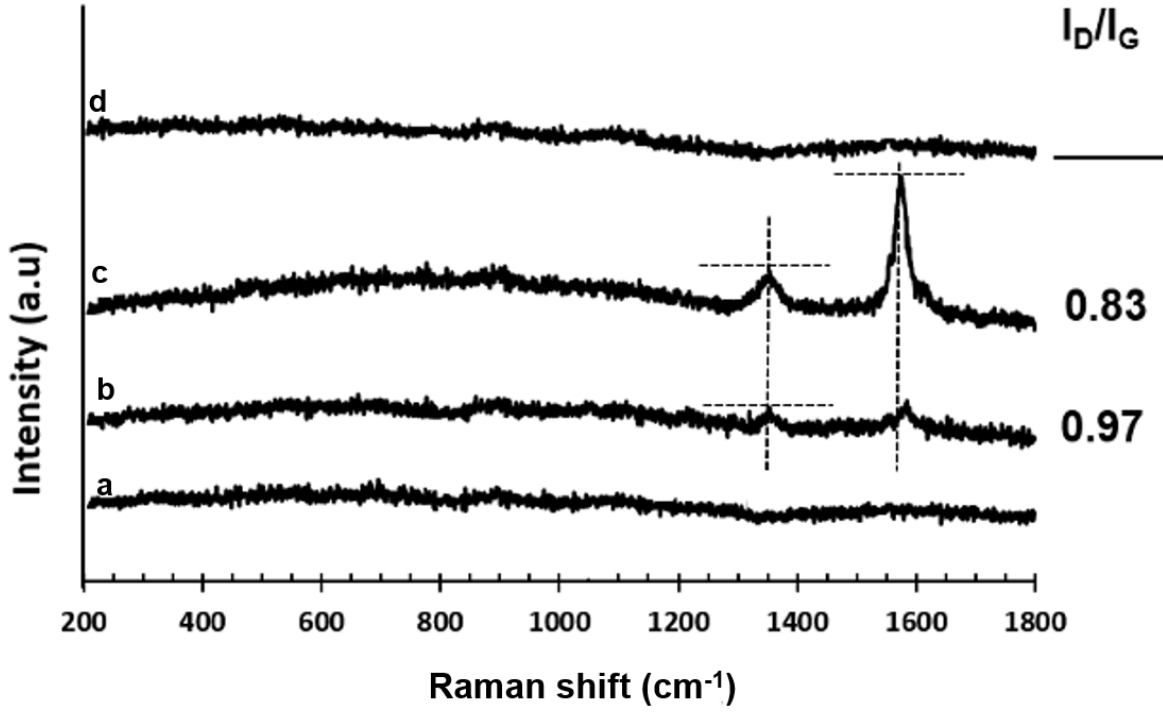


Fig. 9. Raman spectra of unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites sintered at 1000 °C (a) Ti64, (b) Ti64-1%MWCNT_{Gr} (c) Ti64-2%MWCNT_{Gr}, (d) Ti64-3%MWCNT_{Gr}.

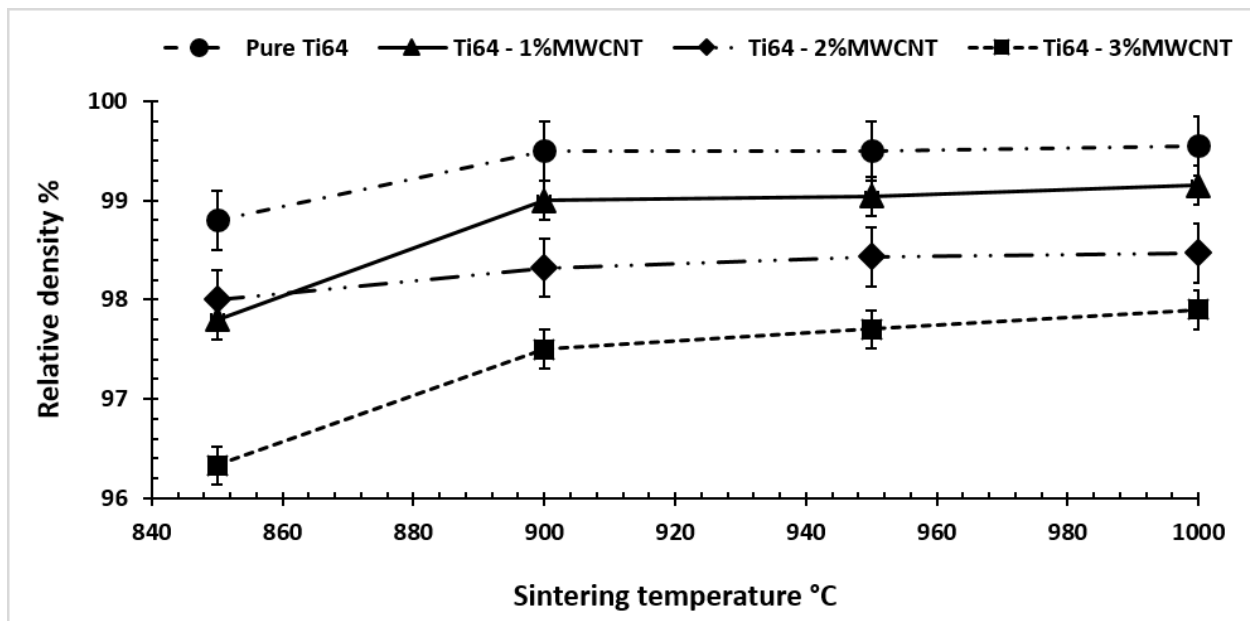


Fig. 10. Densification patterns in unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites.

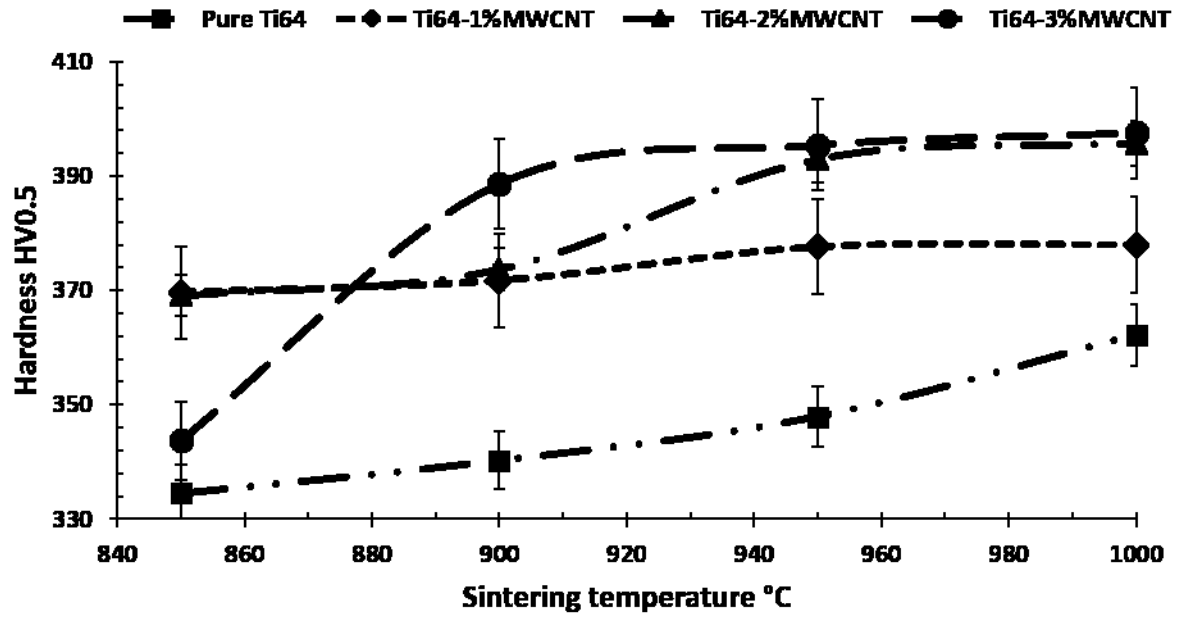


Fig. 11. Microhardness of MWCNT_{Gr}/Ti64 composites with varied weight fractions of MWCNT_{Gr} in Ti64 matrix.

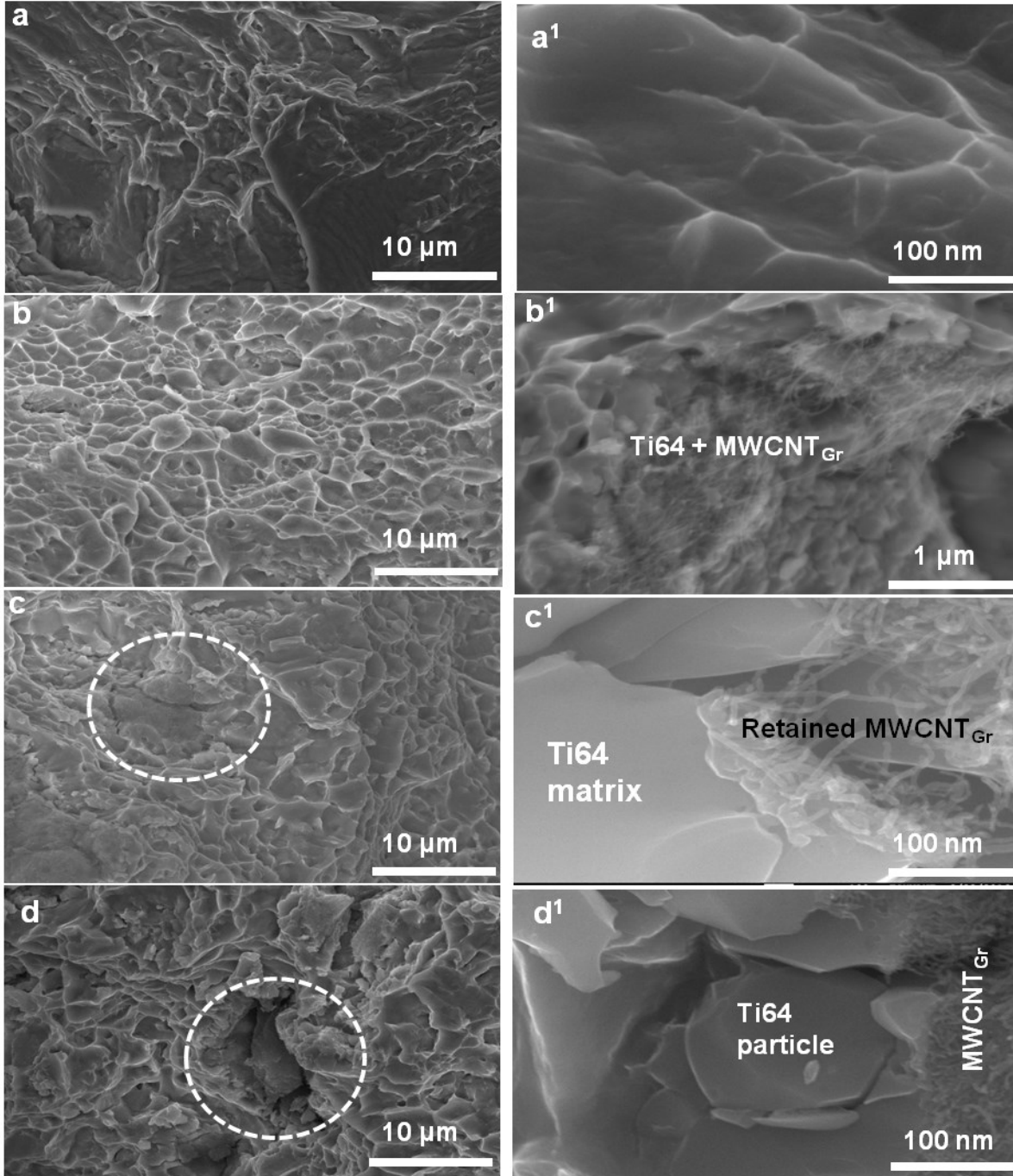


Fig. 12. Fractured surfaces of (a) unreinforced Ti64 and MWCNT_{Gr}/Ti64 composites with varied weight fractions of MWCNT_{Gr} (b) 1 wt % MWCNT_{Gr}, (c) 2 wt % MWCNT_{Gr}, (d) 3 wt % MWCNT_{Gr}, (a¹) – (d¹) are the corresponding SEM images of (a) – (d) taken at higher magnification respectively.

